

**ROCHESTER INSTITUTE OF TECHNOLOGY  
MICROELECTRONIC ENGINEERING**

# Feedback Laboratory

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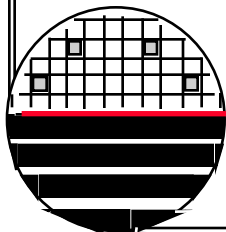
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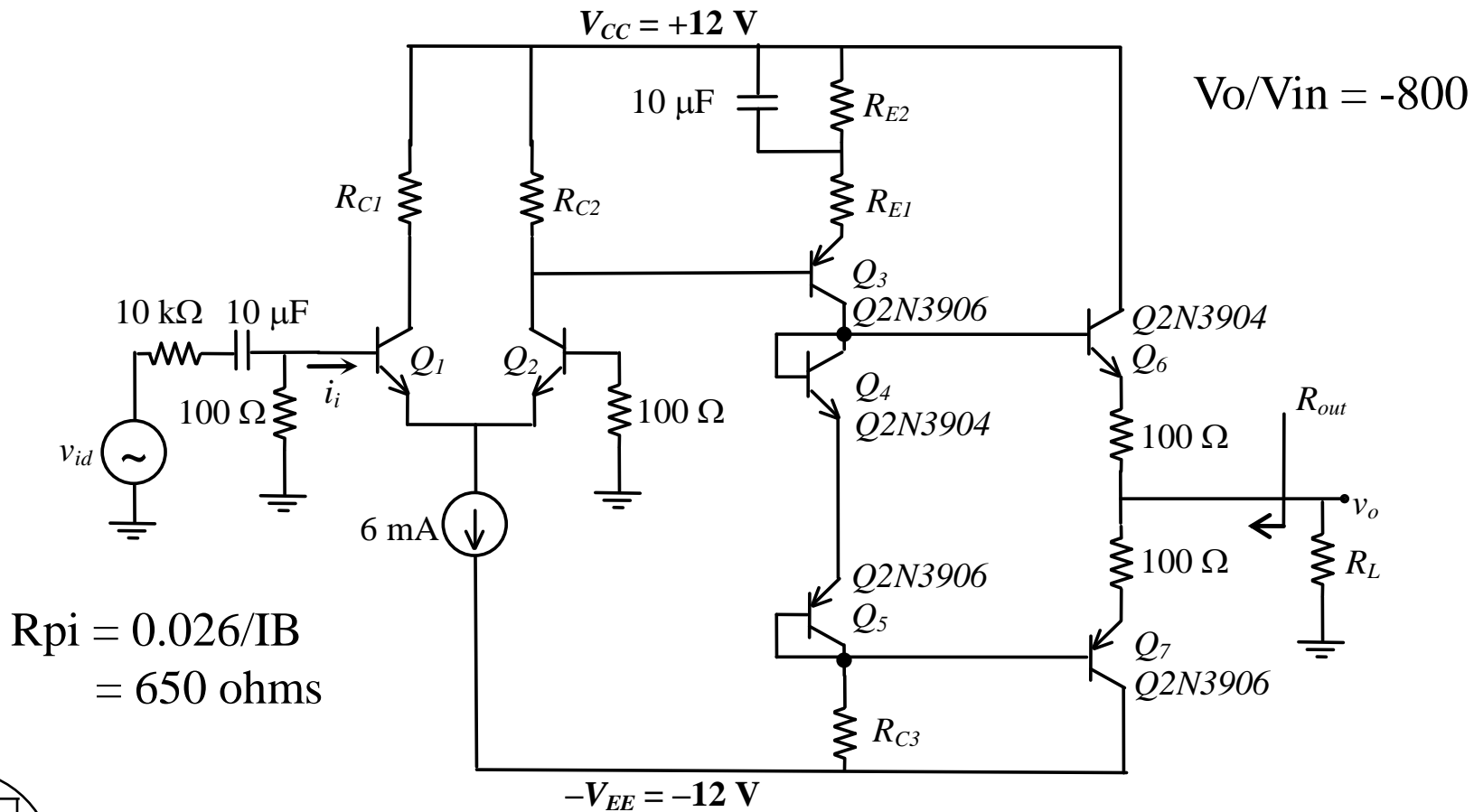
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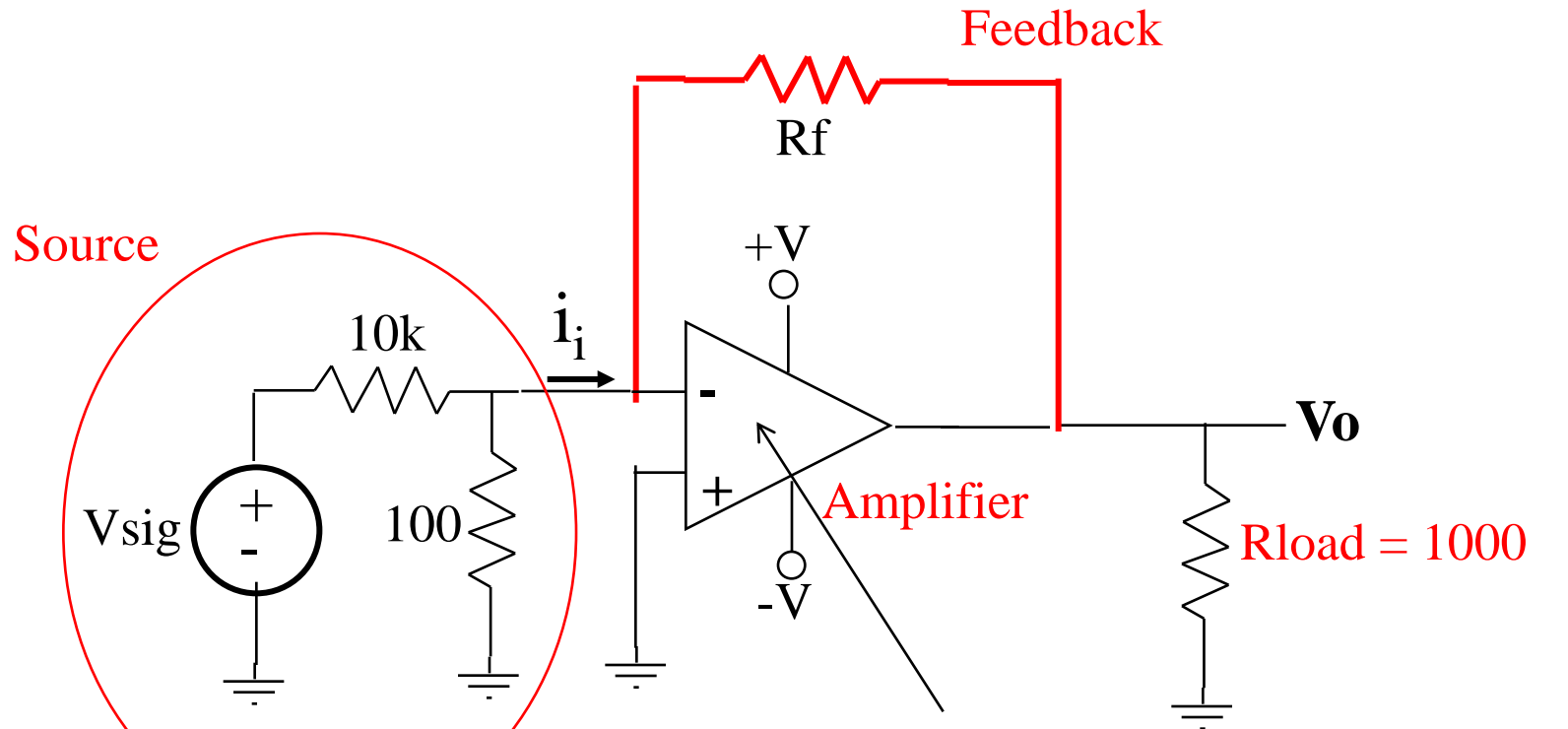


## INTRODUCTION

In the two prior labs we investigated current sources and the differential amplifier (Lab 1) and DC coupled amplifier and output stage (Lab 2). The result was a high gain ( $A_v = -800$ ), low output resistance ( $R_o \sim 100$  ohms) DC amplifier. This lab will add global feedback as shown in the schematic on the following page (a single resistor from output back to the input). This configuration is called Voltage Sampling – Parallel Mixing or Voltage-Shunt feedback. The feedback will result in reduced but less sensitive voltage gain and will modify the input and output resistance. We will predict the results using hand calculations, and SPICE simulations. Then we will construct the circuit and make measurements for the gain with feedback and output resistance.

# MULTISTAGE DIRECT COUPLED AMPLIFIER



**WITH FEEDBACK**

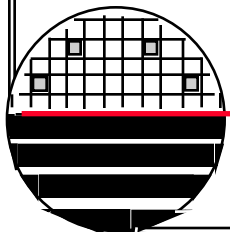
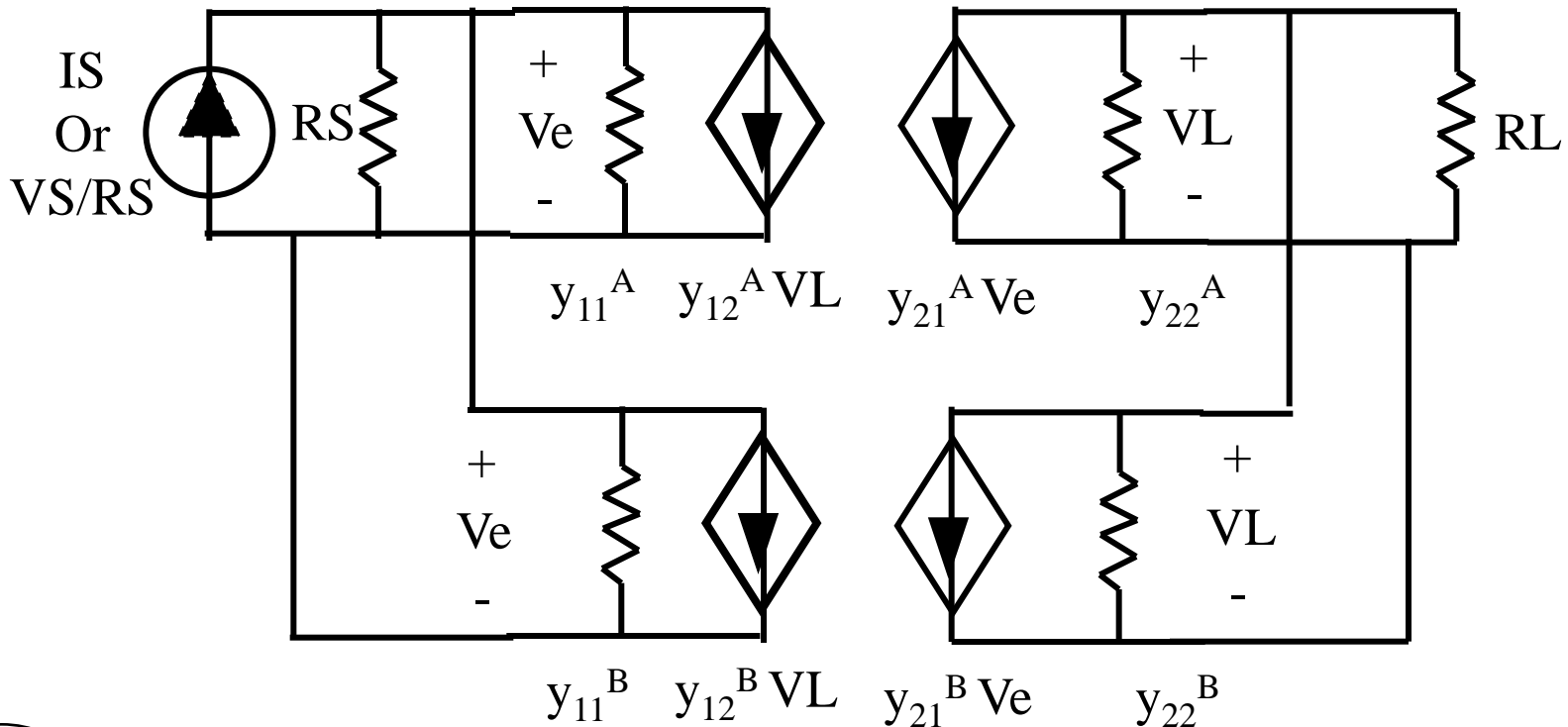
$$A_v = V_o / V_{in} = -800$$

$$R_{in} = R_{pi} + R_{pi} + 100 = 1400$$

$$R_{out} = 100 + \text{few ohms (use 100)}$$

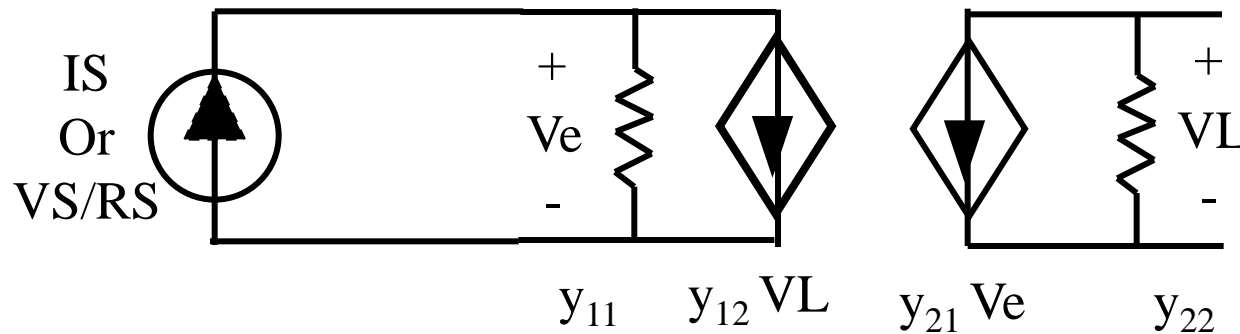
***SMALL SIGNAL AC - VOLTAGE-SHUNT FEEDBACK***

Select y-two port equivalent circuits and Norton equivalent circuits for voltage-shunt feedback:



## SIMPLIFIED VOLTAGE-SHUNT FEEDBACK

From the previous page we combine current sources in parallel and conductances in parallel. (the equivalent circuit is simplified)



$$y_{11} = y_{11}^A + y_{11}^B + 1/R_S$$

$$y_{22} = y_{22}^A + y_{22}^B + 1/R_L$$

$$y_{12} = y_{12}^A + y_{12}^B$$

$$y_{21} = y_{21}^A + y_{21}^B$$

# VOLTAGE-SHUNT FEEDBACK SUMMARY

## Voltage-Shunt

Input Admittance

$$Y_{If} = y_{11} (1 - T)$$

$$Y_{Of} = y_{22} (1 - T)$$

Output Admittance

Loop Gain

$$T = \frac{y_{12}y_{21}}{y_{11}y_{22}}$$

$$A_{Rf} \cong \frac{1}{y_{12}}$$

~ Gain

Exact Gain

$$A_{Rf} = \frac{-y_{21}}{y_{11}y_{22} + y_{12}y_{21}}$$

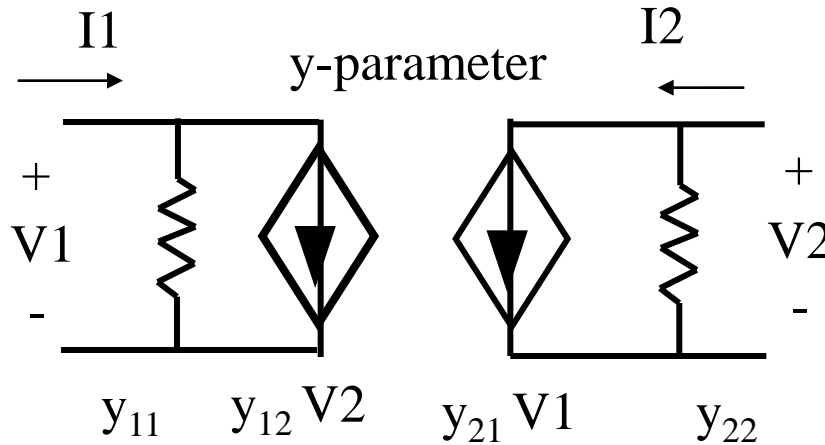
Transresistance

Voltage Gain

$$A_{Vf} = A_{Rf} (1/R_S)$$

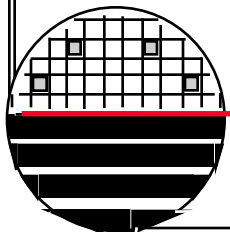
$$A_{If} = A_{Rf} (1/R_L)$$

Current Gain



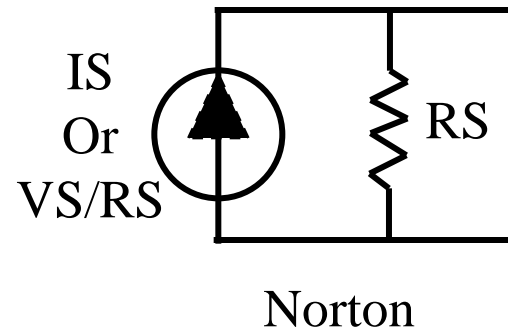
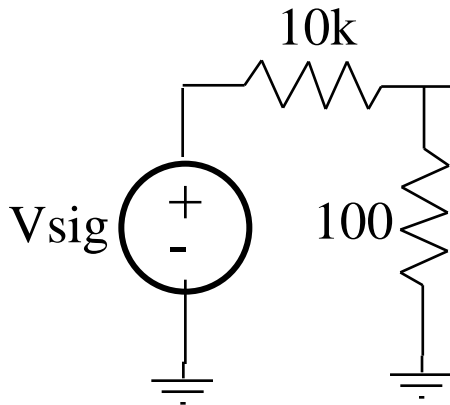
$$I1 = y_{11} V1 + y_{12} V2$$

$$I2 = y_{21} V1 + y_{22} V2$$



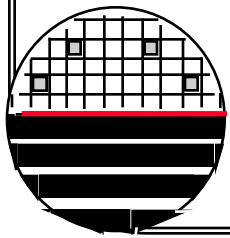
***THE SOURCE***

The source is represented by its Norton equivalent circuit.



$$I_s = V_{sig}/10K$$

$$R_s = 10K // 100 = 99$$



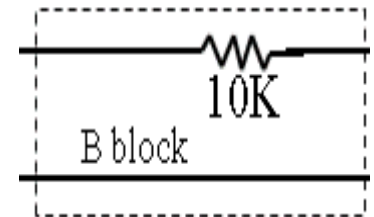
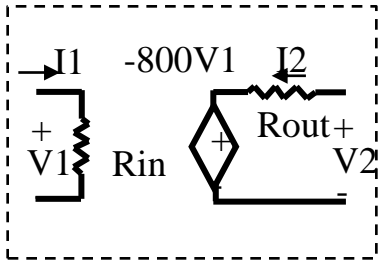
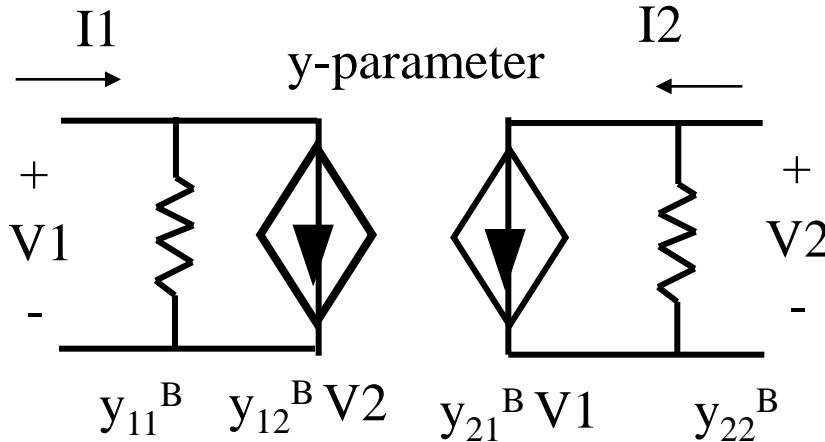


# VOLTAGE-SHUNT FEEDBACK Y PARAMETERS

Find two port parameters for A block and B block.

$$I_1 = y_{11} V_1 + y_{12} V_2$$

$$I_2 = y_{21} V_1 + y_{22} V_2$$



$$y_{11}^A = 1/1400 = 7.14E-4$$

$$y_{12}^A = 0 \text{ (almost always)}$$

$$y_{21}^A = 800/100 = 8$$

$$y_{22}^A = 1/100 = 1E-2$$

$$y_{11}^B = 1/10K = 1E-4$$

$$y_{12}^B = -1/10K = -1E-4$$

$$y_{21}^B = -1/10K = -1E-4$$

$$y_{22}^B = 1/10K = 1E-4$$

**VOLTAGE-SHUNT FEEDBACK**

Find the combined parameters

$$\begin{aligned}
 y_{11} &= y_{11}^A + y_{11}^B + 1/RS &= 7.14e-4 + 1e-4 + 1/99 &= 1.09e-2 \\
 y_{12} &= y_{12}^A + y_{12}^B &= 0 + -1e-4 &= -1e-4 \\
 y_{21} &= y_{21}^A + y_{21}^B &= 8 - 1e-4 &= 8 \\
 y_{22} &= y_{22}^A + y_{22}^B + 1/RL &= 1e-2 + 1e-4 + 1e-3 &= 1.11e-2
 \end{aligned}$$

Compute quantities of interest

Gain with feedback (transresistance)

$$A_{Rf} = \frac{\frac{-y_{21}}{y_{11}y_{22}}}{1 + \frac{-y_{12}y_{21}}{y_{11}y_{22}}} = \frac{\frac{-8}{(1.09e-2)(1.11e-2)}}{1 + \frac{-8(-1e-4)}{(1.09E-2)(1.11e-2)}} = -8680 \text{ ohms}$$

Voltage gain with feedback

$$A_{Vf} = A_{Rf} (1/RS) = -8680 (1/99) = -87.7$$

## VOLTAGE-SHUNT FEEDBACK

Current Gain with Feedback

$$A_{If} = A_{Rf} (1/RL) = -8680 (1/1000) = -8.68$$

Approximate Gain

$$A_{Rf} \sim = 1/y_{12} = -1/1e-4 = -10000 \text{ ohms}$$

$$A_{Vf} \sim = -10000 (1/RS) = -101$$

$$A_{If} \sim = -10000 (1/RL) = -10$$

$$\text{Loop gain} = T = - \frac{y_{12}y_{21}}{y_{11}y_{22}} = (-1e-4)(-8)/(1.09E-2)(1.11E-2) = -6.61$$

## VOLTAGE-SHUNT FEEDBACK

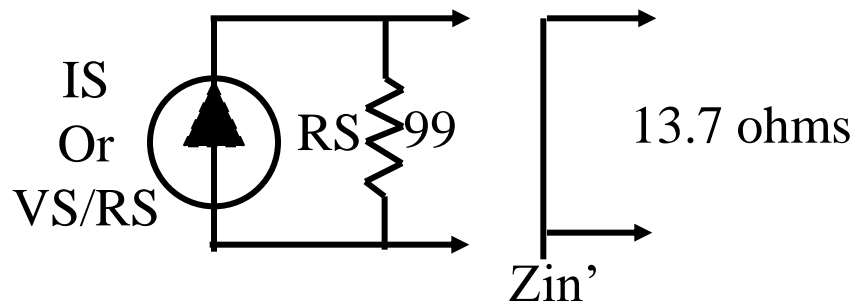
Input admittance  $Y_{if} = y_{11} (1 - T) = y_{11} \left( 1 - \frac{y_{12}y_{21}}{y_{11}y_{22}} \right)$

$$Y_{if} = (1.09E-2)(1 - -6.61) = 82.9 \text{ mS}$$

Input impedance  $Z_{if} = 1/Y_{if} = 12 \text{ ohms}$

Note: this  $Z_{if} = 12 \text{ ohms}$  is equal to the  $99 \text{ ohms}$   $R_S$  in parallel with  $Z_{in}'$  the amplifier input impedance.

So  $99 // Z_{in}' = 12$  therefore we can find  $Z_{in}' = 13.7 \text{ ohms}$



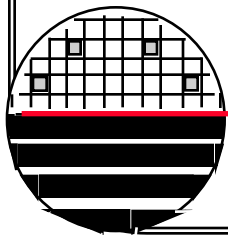
## *VOLTAGE-SHUNT FEEDBACK*

Output Impedance  $Z_{of} = 1/Y_{of}$

$$Y_{of} = y_{22} (1-T) = y_{22} (1 - -2.27) = 82.9 \text{ mS}$$

$$Z_{of} = 1 / Y_{of} = 12 \text{ ohms}$$

Note: this 146 includes the 1000 ohm RL  
so  $Z_{o'}$  (without RL) is = 12.1 ohms



**SUMMARY**

Amplifier Transresistance with no Feedback	1.12Meg ohms
Amplifier Voltage Gain with no Feedback	-800 V/V
Input Resistance with no Feedback	1400 ohms
Output Resistance with no Feedback	100 ohms
Amplifier Transresistance with Feedback	-8680 ohms
Amplifier Voltage Gain with Feedback	-87.7 V/V
Input Resistance with Feedback	13.7 ohms
Output Resistance With Feedback	12.1 ohms
Approximate Transresistance with Feedback	-10,000 ohms
Approximate Voltage Gain with Feedback	-101 V/V

## REFERENCES

1. Sedra and Smith, 5.1-5.4
2. Device Electronics for Integrated Circuits, 2nd Edition, Kamins and Muller, John Wiley and Sons, 1986.
3. The Bipolar Junction Transistor, 2nd Edition, Gerald Neudeck, Addison-Wesley, 1989.

